

The Heat of Vaporization as a Function of Pressure and Temperature

By J. E. HAGGENMACHER

From an analytic expression of the line of saturation of liquids and vapors the heat of vaporization is deduced as a function of pressure and temperature.

The behavior of a two phase system consisting of a liquid and its vapor at equilibrium may be represented by the equation¹

$$P = \frac{RT}{M(v+B)} - \frac{A}{T(v+B)^2} \quad (1)$$

where

$$A = \frac{R^2 T_c^3}{4M^2 P_c}, \quad B = \frac{RT_c}{2MP_c} - v_c$$

For unit mass, p is the pressure; T , the absolute temperature; v , the specific volume; M , the molecular weight; R , the perfect gas constant; and A and B are constants. Subscripts, c , indicate critical values.

Denoting by v_g and v_L the specific volume of saturated liquid and saturated vapor, respectively, there is obtained for the difference of the roots of equation (1)

$$v_g - v_L = \frac{RT}{Mp} \sqrt{1 - \frac{DP}{T^3}} \quad (2)$$

where

$$D = T_c^3/P_c$$

Introducing this expression into the Clapeyron-Clausius equation

$$L = \frac{dp}{dT} T(v_g - v_L)$$

the heat of vaporization, per unit mass, becomes

$$L = \frac{RT^2}{MP} \frac{dp}{dT} \sqrt{1 - \frac{DP}{T^3}} \quad (3)$$

Equation (3) is compared with some calorimetrically measured heats of vaporization.

The vapor pressure and heat of vaporization have been measured for propylene by Powell and Giauque,² for methyl mercaptan by Russell, Osborne and Yost,³ for 1,1,1-trifluoroethane by Russell, Golding and Yost⁴ and for dimethyl sulfide by Osborne, Doescher and Yost.⁵ These authors correlate their vapor pressure data by a relationship of the form

$$\log P_{\text{mm}} = -\frac{a}{T} - b \log T + c$$

Then

$$\frac{dp}{dT} = \frac{P}{T^2} (2.303a - bT)$$

Taking p in atmospheres, T in °K. (ice-point 273.16), $R = 0.08206$, and 1 liter-atm. = 24.206

(1) Haggenmacher, THIS JOURNAL, **66**, 313 (1944); **68**, 1123 (1946); *Phys. Rev.*, **69**, 242 (1946).

(2) Powell and Giauque, *ibid.*, **61**, 2366 (1939).

(3) Russell, Osborne and Yost, *ibid.*, **64**, 165 (1942).

(4) Russell, Golding and Yost, *ibid.*, **66**, 16 (1944).

(5) Osborne, Doescher and Yost, *ibid.*, **64**, 169 (1942).

g-cal., the heat of vaporization from equation (3), becomes

$$L = (4.5737a - 1.9863bT) \sqrt{1 - \frac{Dp}{T^3}} \text{ g. cal./mole} \quad (4)$$

The vapor pressure and heat of vaporization of dimethyl ether have been measured by Kennedy, Sagenkahn and Aston.⁶ Their vapor pressure equation is of the form

$$\log P_{\text{mm}} = -\frac{a}{T} + b \log T - cT + d$$

Then

$$\frac{dp}{dT} = 2.303 \frac{P}{T^2} \left(a + \frac{bT}{2.303} - cT^2 \right)$$

and from equation (3)

$$L = 4.5737 \left(a + \frac{bT}{2.303} - cT^2 \right) \sqrt{1 - \frac{Dp}{T^3}} \text{ g. cal./mole} \quad (5)$$

Inserting for the constants a , b and c the numerical values given by the authors cited the heats of vaporization have been calculated and are compared with the measured ones in Table I.

TABLE I

Substance	T , °C.	p , atm.	L , g-cal./mole meas.	L , g-cal./mole eq. (4)	L , g-cal./mole eq. (5)
Propylene	-47.75	1.0000	4402	4346	
Methylmercaptan	5.96	1.0000	5872	5833	
1,1,1-Trifluoroethane	-48.76	0.9339	4583	4607	
Dimethyl sulfide	17.90	0.4809	6688	6664	
Dimethyl ether	-24.80	1.0000	5141	5101	
Benzene	20	0.0982	(8123) ^a	8146	
	50	.3539	7756	7729	
	80	.9916	7355	7306	
	110	2.300	6914	6841	
	130	3.717	(6594)	6497	

* Values in parentheses are extrapolated.

For benzene the vapor pressure data of E. R. Smith⁷ and the measurements of the heat of vaporization of Flock, Ginnings and Holton⁸ have been used.

The Smith formulation of the vapor pressure is of the form

$$\log P_{\text{mm}} = -\frac{a}{b+i} + c$$

Then, changing from °C. to °K.

$$\frac{dP}{dT} = \frac{2.303 aP}{(T+b-273.16)^2}$$

and from equation (3), upon inserting for a and b the values given by Smith,

$$L = \frac{70.923T^2}{(T-52.29)^2} \sqrt{1 - \frac{Dp}{T^3}} \text{ g-cal./mole} \quad (6)$$

(6) Kennedy, Sagenkahn and Aston, *ibid.*, **63**, 2267 (1941).

(7) E. R. Smith, *J. Research Natl. Bur. Standards*, **26**, 129 (1941).

(8) Flock, Ginnings and Holton, *ibid.*, **6**, 881 (1931).

The heats of vaporization calculated from equation (6) are compared with the measurements of Fiock, Ginnings and Holton in Table I.

For water the data of Smith, Keyes and Gerry⁹ for the vapor pressure, and the values of Osborn and Meyers¹⁰ for the rate of change of the vapor pressure, have been used. The heats of vaporization calculated from equation (3) are compared with the values given by Osborn, Stimson and Ginnings¹¹ in Table II.

TABLE II
HEAT OF VAPORIZATION OF WATER

T_1 °C.	L_1 , g. cal./g. O.S.G. eq. (3)	T_2 °C.	L_2 , g. cal./g. O.S.G. eq. (3)	T_3 °C.	L_3 , g. cal./g. O.S.G. eq. (3)
0	596.5	596.7	140	512.0	515.6
20	585.6	586.5	160	497.1	500.9
40	574.5	575.8	180	480.9	485.3
60	563.1	564.7	200	463.1	467.5
80	551.2	553.3	220	443.5	448.0
100	538.9	541.5	240	421.5	425.9
120	525.9	529.0	260	396.6	400.9
				374.11	0

Heats of vaporization may also be determined from equation (3) in the absence of an analytic correlation of the vapor pressure data. Given a sufficient number of experimental points an

(9) Smith, Keyes and Gerry, *Proc. Am. Acad. Arts Sci.*, **69**, 137 (1934).

(10) Osborn and Meyers, *J. Research Natl. Bur. Standards*, **1**, 1 (1934).

(11) Osborn, Stimson and Ginnings, *Mech. Eng.*, **57**, 162 (1935).

approximation for dp/dT is obtained from

$$\left. \frac{dp}{dT} \right|_{T_2} \cong \left. \frac{\Delta P}{\Delta T} \right|_{T_2} = \frac{P_3 - P_1}{T_3 - T_1}$$

where, geometrically, the slope of the chord between the points p_1, T_1 and p_3, T_3 is taken for the slope of the tangent line at p_2, T_2 . The accuracy of the method, clearly, depends upon the narrowness of the spacing of the experimental points. A very useful method of evaluating dp/dT has been proposed by Rutledge.¹² His formulations permit simple application but require equal intervals of either p or T . Both methods are suitable for calculating the rate of change of the vapor pressure since in its entire range the vapor pressure curve is devoid of abrupt directional changes and points of inflection.

Summary

A function of pressure and temperature is derived for the heat of vaporization.

The equation is applicable to all substances whose critical pressure and critical temperature are known and for which vapor pressure data are available.

(12) Rutledge, *Phys. Rev.*, **40**, 262 (1932), and Margenau and Murphy, "The Mathematics of Physics and Chemistry," D. Van Nostrand Co., New York, N. Y., 1943, p. 456.

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Heat Capacities at Low Temperatures of Na_2TiO_3 , $\text{Na}_2\text{Ti}_2\text{O}_5$ and $\text{Na}_2\text{Ti}_3\text{O}_7$ ¹

BY C. HOWARD SHOMATE²

The thermodynamic properties of certain titanates are of interest in connection with experimental studies of methods of treatment and utilization of titaniferous iron ores. Data for the sodium titanates are particularly pertinent to the smelting of such ores under a slag rich in sodium carbonate.

A recent paper³ from the Pacific Experiment Station of the Bureau of Mines presented low temperature heat capacity and entropy data for ferrous, calcium, and magnesium metatitanates. This paper reports similar data for three titanates of sodium. No previous low-temperature values exist for these substances, but Naylor⁴ has determined their high-temperature heat contents.

Materials

The titanates were prepared in this Laboratory by R. J. O'Dea² by repeated heating of stoichiometric amounts of sodium carbonate and titanium dioxide at 900 to 1,100° for several hours with continuous pumping to remove carbon dioxide.

Analyses of the final products for titanium and carbon dioxide, and the known silica impurity of the original titanium dioxide, indicated the following proximate compositions: 98.4% Na_2TiO_3 , 1.1% Na_2SiO_3 and 0.5% Na_2CO_3 ; 98.7% $\text{Na}_2\text{Ti}_2\text{O}_5$, 1.0% Na_2SiO_3 and 0.3% Na_2CO_3 ; 98.6% $\text{Na}_2\text{Ti}_3\text{O}_7$, 1.1% Na_2SiO_3 and 0.3% Na_2CO_3 .

X-Ray examinations of the samples were made by Dr. E. V. Potter.⁵ The crystalline character of the substances was proved, but there were no previous data with which to check the diffraction patterns.

Heat Capacities

The method and apparatus used in the low-temperature heat capacity measurements were described previously.^{6,7} The experimental results, expressed in defined calories (1 calorie =

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(2) Chemist, Pacific Experiment Station, Bureau of Mines.

(3) Shomate, *THIS JOURNAL*, **68**, 964 (1946).

(4) Naylor, *ibid.*, **67**, 2120 (1945).

(5) Physicist, Salt Lake City Station, Bureau of Mines.

(6) Kelley, *THIS JOURNAL*, **63**, 1137 (1941).

(7) Shomate and Kelley, *ibid.*, **66**, 1490 (1944).